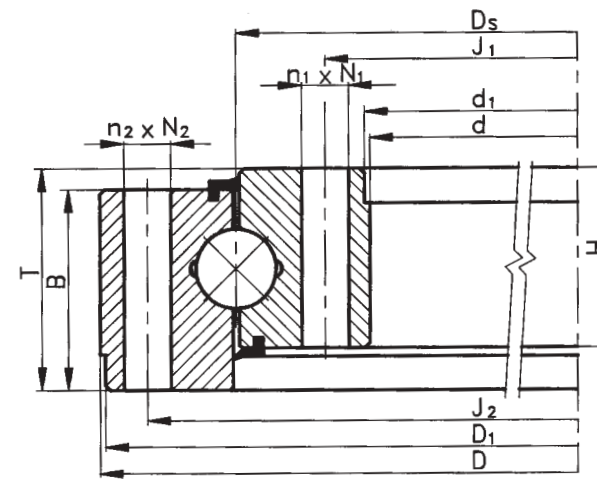


# FOUR-POINT CONTACT SLEWING RINGS

- without gear [ O ]



Number of the Loading Curve	Boundary Dimensions			Static Ax. Basic Load Rating $C_{0a}$	Designation	Weight $G$	Abutment Dimensions				Other Specifications				Note No	Notes	
	$d$	$D$	$T$				$J_1$	$J_2$	$N_1$	$N_2$	$n_1$	$n_2$	$d_1$	$D_1$			$H$
	[mm]			[kN]		[kg]	[mm]										
1	140	300	36	359	90-1B13-0220-0318	11.3	170	270	18	M16	12	12	-	-	30	30	
2	145	300	50	440	90-1B20-0223-0326	15	175	270	17	17	15	16	-	-	44	44	1
3	145	300	50	440	90-1B20-0223-0427	16.7	175	270	14.27	14.27	16	16	-	-	44	44	
4	145	300	50	440	90-1B20-0223-0447	17	175	270	1/2-13 UNC	14.27	8	8	146	-	44	44	2
5	145	300	50	527	90-1B22-0223-0397	16.5	175	270	17	5/8-11 UNC	15	16	146	-	44	44	1
6	183	375	63	720	90-1B25-0279-0428	33.5	220	338	M16	M16	12	12	185	373	54	54	
7	200	300	35	332	90-1B14-0250-0479	8	220	280	M10	M10	16	16	-	-	30	30	
8	210	365	40	594	90-1B20-0289-0295	20	240	335	14	14	16	16	-	-	38	38	
9	210	365	40	594	90-1B20-0289-0295-1	18	240	335	1/2-13 UNC	1/2-13 UNC	19	16	-	-	38	38	3
10	270	486	63	1027	90-1B25-0378-0401	50	314	442	22	M20	16	16	-	-	54	54	
11	323.6	520.29	54.1	1140	90-1B25-0422-0485	46.5	365.125	479.425	17.5	5/8-11 UNC	20	20	-	-	52.3	52.3	4
12	323.6	520.29	54.1	1140	90-1B25-0422-0513	47	365.125	479.425	5/8-11 UNC	16.7	20	20	-	-	52.3	52.3	5;6
13	333	558	72	1469	90-1B30-0446-0502	66	377	514	22	22	20	20	-	-	63	63	
14	336	474	46	851	90-1B20-0405-0387	25	360	450	14	14	30	30	-	-	41	41	
15	384	562	59	1307	90-1B25-0475-0204	47	420	530	18	18	16	16	-	560	52	52	
16	400	580	70	1642	90-1B30-0490-0377	57	430	550	17	M16	18	18	-	-	61	61	
17	400	610	76	1666	90-1B30-0506-0420	76	440	570	18.3	18.3	24	24	410	600	66	66	7
18	450	650	75	1951	90-1B32-0550-0418	69	485	615	22	22	36	35	-	-	65	65	8
19	460	699	72	2040	90-1B32-0580-0342	93	504	655	22	22	22	22	-	-	63	63	
20	468	704	86	2609	90-1B40-0586-0337	108	508	664	22	22	36	35	-	-	79	79	8;9
21	545	730	68	1785	90-1B25-0640-0355	73	580	690	17.5	M12	24	24	-	-	53	59	
22	634	848	56	1605	90-1B20-0744-0341	75	662	820	M18x1.5	M18x1.5	24	24	-	-	45.5	45.5	
23	810	900	40	1274	90-1B13-0854-0313	27	826	884	9	9	24	24	-	-	33	33	
24	872	1016	56	2033	90-1B20-0941-0357 S	70	898	990	M12	M12	24	24	874	1014	46	46	
25	878.6	1121	74	3425	90-1B30-1000-0380	162	925	1075	22	22	24	24	880	1120	63.5	63.5	
26	964	1218	56	2827	90-1B22-1094-0207	142	1012	1170	M16	M16	36	36	-	-	45.5	45.5	
27	2200	2400	73	6588	90-1B25-2300-0107	300	2240	2360	22	22	60	60	-	-	63	63	

## Mouting Procedure

Before assembling it is necessary to clean all surfaces thoroughly from burrs, paint residues, etc. Seating surfaces should be dry, without lubricant. Furthermore it is necessary to inspect flatness of the seating surfaces. Feeler gauges are used to check slewing ring adaptation.

The unhardened area of the non rotating ring should be mounted so that it is positioned in the least loaded zone - i.e. in the plane perpendicular to the main load plane.

The unhardened area is marked on the respective ring non-functional surface with symbol "X" by stamping or with a red line.

When assembling a geared slewing ring it is important to adjust the backlash in the gear correctly. It is adjusted with a feeler gauge or with another suitable method in the zone of maximum radial gear runout. The extent of the backlash should be in the range of (0.035-0.04).m, where "m" means the gear module. The backlash should be inspected again after the slewing ring is finally fixed on the machine. The zone of the maximum radial gear runout is marked with a blue line in the gap between teeth.

Slewing rings are fixed on the machine with pre-stressed bolts. Before assembly the mounting bolts should be coated slightly with oil. The necessary tightening torque for corresponding bolt size and material is indicated in Table 1.

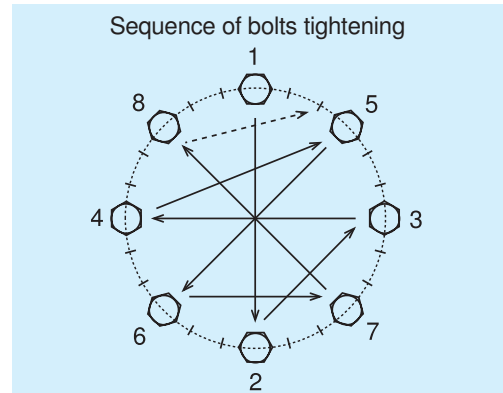
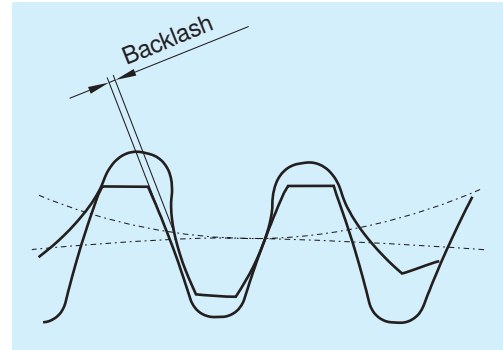


Table 1

Bolt Thread Size	Bore Diameter [mm] DIN/ISO 273	Tightening torque at $\mu = 0.14$ [Nm]	
		Rigidity Class of Bolt 8.8	Rigidity Class of Bolt 10.9
M 12	14	78	117
M 14	16	126	184
M 16	17.5	193	279
M 18	20	270	387
M 20	22	387	558
M 24	26	666	954
M 27	30	990	1395
M 30	33	1350	1890
		Grade 5	Grade 8
UNC 5/8"-11	18	180	260
UNC 3/4"-10	21	320	460
UNC 7/8"-9	25	520	730
UNC 1"-8	27.5	770	1100
UNC 1 1/8"-7	32	970	1560
UNC 1 1/4"-7	35	1370	2190
		Grade 5	Grade 8
UNF 5/8"-18	18	210	290
UNF 3/4"-16	21	360	510
UNF 7/8"-14	25	580	820
UNF 1"-12	27.5	860	1210
UNF 1 1/8"-12	32	1100	1760
UNF 1 1/4"-12	35	1520	2440

## Slewing Ring Inspection in Operation

During service it is necessary to regularly recheck the fixing bolts torque at the in recommended intervals. Individual inspection intervals vary according to machine operation conditions.

When inspecting, the following method can be used (approximately valid for crane operation):

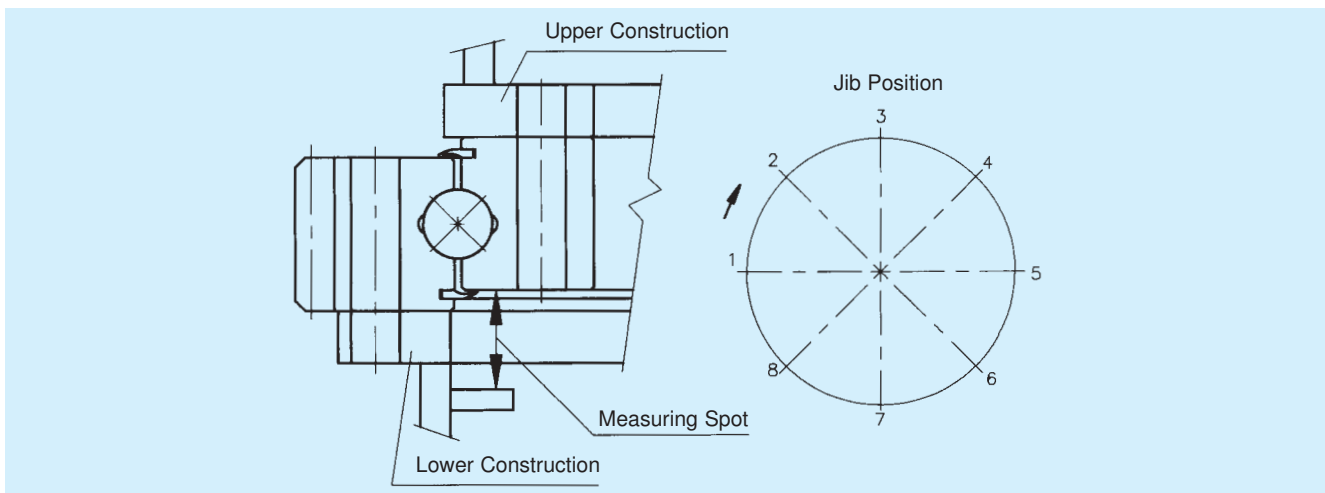
Inspection No.	Number of Operating Hours	Inspecting Action
1.	About 200 Hours	- inspection of all bolts torque - if more than 10% of bolts are loose, another inspection is necessary after about 200 operating hours
2.	About 600 Hours	- inspection of all bolts torque
3. and further	After about 2 000 Hours	- if one or more bolts are loose to less than 80% of the prescribed torque, these and both adjoining bolts must be replaced by new ones - if 20% of all bolts have less than 80% of prescribed torque, all bolts must be replaced by new ones
	Each 12 000 Hours	- replace all bolts by new ones

Note: Specified inspection intervals must be shortened by 1/2 up to 1/3 for machines loaded more heavily by vibrations or dynamically.

In addition to the fixing bolts check, raceway wear checking is also carried out in operation ( mainly at significant important rotary connections) using the measurement method "tilting clearance". The tilting clearance is the difference of the mutual ring displacement in axial direction measured under load by minimum and maximum tilting moment. In the operation register of the equipment the initial tilting clearance is recorded (in the jib position 1 to 8) and its enlargement is then followed in certain time intervals. The principle of the tilting clearance measurement and an example of the measuring record are shown in Figure 3.

More detailed technical information concerning slewing ring checking can be provided by the experts of PSL, Technical Consultancy Department.

Figure 3



## Slewing Ring Tables

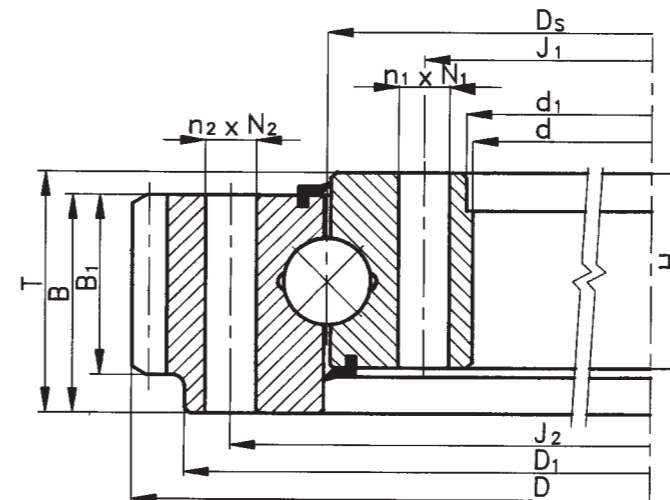
The following Tables (pages 14 - 27) show the standard PSL slewing rings whose cross-section corresponds to the figure above the Table. Any deviations are specified in the notes.

Further Tables (pages 28 - 30) show special slewing rings whose cross-section does not correspond to the figures over the Tables, or they differ from the standard design (e.g. they have irregular spacing of the fastening holes, special gear, higher tolerance class, are non-sealed from one or both sides, or have non-standard shape of the rings, etc.). More detailed information concerning these slewing rings can be provided by the experts of the PSL Technical Consultancy Department, address - see page 2.

The tables of the special slewing rings show some types designated by the designation PSL 912-... They are slewing rings of the old three-ring design (one ring is split).

# FOUR-POINT CONTACT BALL SLEWING RINGS

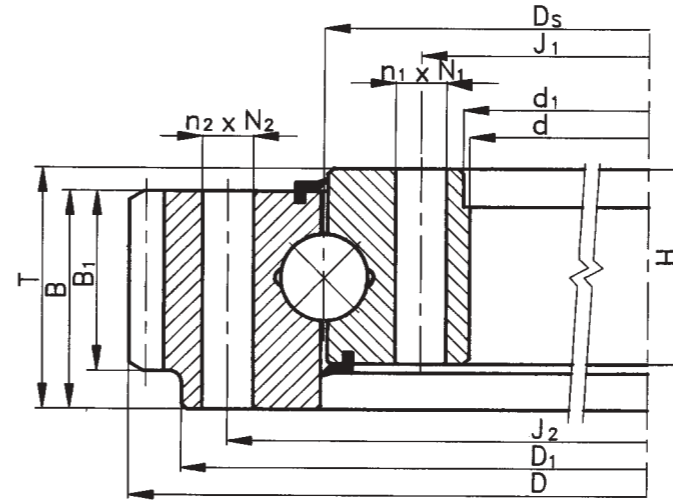
-with external gear [ E ]



Number of the Loading Curve	Boundary Dimensions			Static Ax. Basic Load Rating $C_{0a}$	Designation	Weight G	Abutment Dimensions					Other Specifications										Permissible circumferencial force		Note No	Notes
	d	D	T				$J_1$	$J_2$	$N_1$	$N_2$	$n_1$	$n_2$	$d_1$	$D_1$	H	B	$B_1$	m(DP)	z	x	$F_{TDov}$	$F_{TmaxDov}$			
	[mm]			[kN]		[kg]	[mm]					[mm]										[kN]			
28	145	316.58	50	440	9E-1B20-0221-0493	16.5	175	270	5/8-11 UNC	5/8-11 UNC	16	16	-	-	44	44	44	(5)	60	-	16	33	1	1 Right-hand helical gear $\alpha = 20^\circ$ ; $\beta = 6^\circ$	
29	145	316.6	50	440	9E-1B20-0223-0201	16.5	175	270	5/8-11 UNC	5/8-11 UNC	15	16	-	-	44	44	44	5	61	-	16	32	2; 3	2 Right-hand helical gear $\alpha = 14^\circ 30'$ ; $\beta = 6^\circ$	
30	145	316.6	50	440	9E-1B20-0223-0282	16.5	175	270	5/8-11 UNC	5/8-11 UNC	15	16	-	-	44	44	44	5	61	-	16	32	2; 3	3 Fixing holes on inner ring are divided on the circumference with spacing $a' 360^\circ/16$	
31	145	312	50	440	9E-1B20-0223-0287	16.5	175	270	5/8-11 UNC	5/8-11 UNC	15	16	-	-	44	44	44	(5/7)	60	-	19	39	3; 4	4 Gear Fellows Stub $\alpha = 20^\circ$	
32	171	318.6	40	441	9E-1B17-0235-0182	13	195	275	13	13	12	12	173	-	35	35	35	4	78	-	10	20		5 Fixing holes on inner ring are divided on the circumference with spacing $a' 360^\circ/28$	
33	235	403.5	55	742	9E-1B22-0308-0443	23.5	259	358	13	13	27	30	-	330	46	46	42	5	79	-	16	32	5; 6	6 Centering diameter is on the opposite bearing face	
34	263.5	434.08	50	849	9E-1B22-0344-0396	29	295	390	5/8-11 UNC	5/8-11 UNC	23	18	-	-	44	44	44	(5/7)	84	-	20	41	4; 7	7 Fixing holes on inner ring are divided on the circumference with spacing $a' 360^\circ/24$	
35	265	433.5	50	714	9E-1B20-0345-0273	25.5	295	390	5/8-11 UNC	5/8-11 UNC	24	18	-	-	43	43	43	(5/7)	84	-	20	40	4	8 Gear Involute Stub $\alpha = 20^\circ$	
36	265	433.5	50	714	9E-1B20-0345-0286	25.5	295	390	5/8-11 UNC	17	24	18	-	-	43	43	43	(5/7)	84	-	20	40	4	9 Non-through tapped fixing holes on both rings	
37	265	433.9	50	714	9E-1B20-0343-0311	28.5	295	390	14	1/2-13 UNC	8	9	-	-	44	44	44	(5/7)	84	-	20	41	4	10 Gear Fellow Stub Tooth System Special-Full Fillet Radius $\alpha = 20^\circ$	
38	265	437.34	50	708	9E-1B20-0343-0492	25.5	295	390	5/8-11 UNC	5/8-11 UNC	24	18	-	-	44	44	44	5	85	-	17	34	2	11 Fixing holes on inner ring are divided on the circumference with spacing $a' 360^\circ/36$	
39	323.7	520.3	54	1140	9E-1B25-0422-0354	46	365.1	479.4	5/8-11 UNC	5/8-11 UNC	20	20	-	-	52.3	52.3	52.3	(5/7)	101	-	25	51	4	12 Fixing holes on inner ring are recessed on $\varnothing 50$ into the depth of 6.35	
40	323.7	537.21	57.15	1140	9E-1B25-0422-0477	47	365.1	479.425	20.65	3/4-10 UNC	16	18	-	-	50.8	50.8	50.8	(4)	83	-	24	49	8; 9	13 Non-through tapped fixing holes on outer ring	
41	323.85	520.14	54.1	1140	9E-1B25-0422-0481	46	365.125	479.425	5/8-11 UNC	5/8-11 UNC	20	20	-	-	52.3	52.3	52.3	(5/7)	101	-	25	51	9; 10	14 Fixing holes on both rings ring are recessed on $\varnothing 30$ into the depth of 19.1	
42	324	527.8	60	1043	9E-1B22-0422-0516	48	365	479.4	M16	M16	20	20	-	-	51	51	51	5	103	-	20	41	2; 9	15 Gear Agma Stub $\alpha = 20^\circ$	
43	383	589.5	75	1646	9E-1B32-0475-0470	58.5	410	540	16	16	35	36	384	565	63	60	52	4.5	129	-	12	24	11	16 Fixing holes on inner ring are divided on the circumference with spacing $a' 360^\circ/30$ (two places $a' 180^\circ$ are not occupied)	
44	428.75	721.36	104.65	2778	9E-1B45-0572-0522	166	473.075	644.525	24	3/4-10 UNC	23	24	431.8	692.15	87.38	98.55	82.55	(4)	112	-	41	83	7; 8; 12; 13	17 Fixing holes on inner ring are recessed on $\varnothing 21$ into the depth of 11.5	
45	431.8	721.36	88.9	2470	9E-1B40-0559-0390	141	473.075	644.525	20.6	20	23	18	-	-	81	81	81	(4)	112	-	49	98	7; 14; 15	18 Fixing holes on inner ring are divided on the circumference with spacing $a' 360^\circ/30$	
46	431.8	721.36	87	2470	9E-1B40-0559-0457	138	472.948	644.525	20	20	28	24	-	-	82	82	82	(4)	112	-	41	83	8; 14; 16	19 Fixing holes on inner ring are divided on the circumference with spacing $a' 360^\circ/30$	
47	545	765.4	68	1785	9E-1B25-0640-0150	84	580	700	17.5	M16	24	24	-	-	53	59	59	8	92	+1	45	91	13	20 Fixing holes on outer ring are recessed on $\varnothing 41.3$ into the depth of 28.6	
48	552.45	816	123.9	2434	9E-1B32-0678-0430	167	604.012	753	20.5	20.5	35	36	-	786	92	92	82.5	6	132	+1.0922	57	114	11	21 Gear Involute Stub-Full Fillet radius $\alpha = 20^\circ$	
49	556	742.3	53.5	1382	9E-1B20-0644-0208	51	595	685	13.5	M12	44	44	-	-	44.5	44.5	44.5	6	122	-	21	42	17	22 Fixing holes on inner ring are divided on the circumference with spacing $a' 360^\circ/40$	
50	667	888	69	2122	9E-1B25-0762-0321	107	703	819	17.5	M16	32	32	-	-	57	60	60	8	108	+0.6	56	111	13	23 Fixing holes on both rings ring are recessed on $\varnothing 34$ into the depth of 16	
51	714.37	981.71	125.4	4275	9E-1B45-0857-0407	261	762	908.05	7/8-14 UNC	7/8-14 UNC	24	20	720.725	952.5	98.55	122.25	88.9	(4/5)	153	-	65	130	4; 9		
52	717.55	981.71	124.97	4275	9E-1B45-0854-0343	253	762	908.05	28.575	1-8 UNC	29	24	720.85	952.5	95.25	115.06	83.06	(4/5)	153	-	60	121	4; 13; 18		
53	717.55	981.71	124.97	4275	9E-1B45-0854-0343-1	250	762	908.05	1-8 UNC	1-8 UNC	35	36	720.85	952.5	95.25	115.06	83.06	(4/5)	153	-	60	121	4; 9; 11		
54	730	1006.6	98	3385	9E-1B35-0845-0476	196	770	920	M20	M20	20	20	-	965	79	80	70	8	122	+1	64	129			
55	778	1102	80	4141	9E-1B40-0910-0345	205	830	990	26	26	39	40	780	-	72	72	72	12	89	+0.5	100	200	19		
56	806.45	1155.7	125.5	4802	9E-1B45-0947-0484	371	854.456	1038.86	11/8 - 12 UNC	27.5	29	30	812.8	1089.66	98.6	122.25	88.9	(2)	89	-	106	212	18; 20		
57	812.8	1072.9	92.2	3355	9E-1B32-0924-0503	195	850.9	993.775	3/4-16 UNF	3/4-16 UNF	36	36	-	1030.22	68.33	82.55	76.2	(2.5)	104	-	74	148	21		
58	885	1173.6	82	3662	9E-1B32-1000-0223	195	929	1070	22	22	51	52	-	-	68	68	68	12	95	+0.5	78	157	22		
59	889	1082.8	82	2768	9E-1B25-0984-0451	140	922.02	1014.98	17.5	5/8-11 UNC	30	30	-	-	74.7	73.7	73.7	(2.5)	105	-	71	143	13		
60	955	1324	137	5597	9E-1B45-1105-0329	480	1010	1200	26	M24	42	42	960	1260	117	122	100	14	91	+0.93	154	308	13		

# FOUR-POINT CONTACT BALL SLEWING RINGS

-with external gear [ E ]  
(continued)

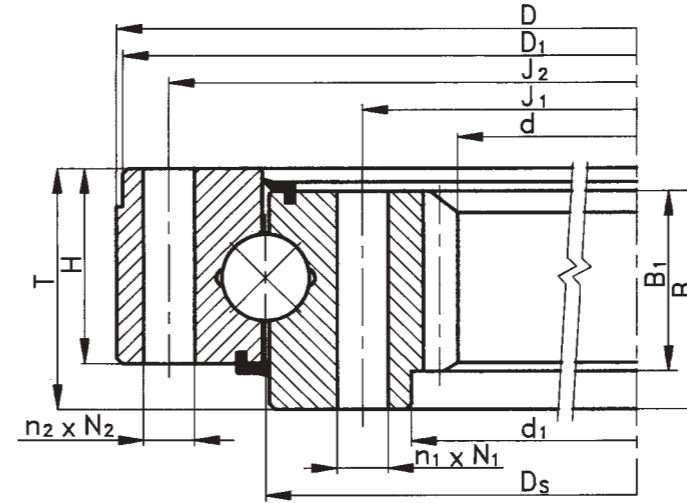


Number of the Loading Curve	Boundary Dimensions			Static Ax. Basic Load Rating $C_{0a}$	Designation	Weight G	Abutment Dimensions					Other Specifications										Permissible circumferencial force		Note No	Notes
	d	D	T				J <sub>1</sub>	J <sub>2</sub>	N <sub>1</sub>	N <sub>2</sub>	n <sub>1</sub>	n <sub>2</sub>	d <sub>1</sub>	D <sub>1</sub>	H	B	B <sub>1</sub>	m(DP)	z	x	F <sub>TmaxDov</sub>	F <sub>TDov</sub>			
	[mm]			[kN]		[kg]	[mm]					[mm]										[kN]			
61	991.36	1396.746	120.65	7462	9E-1B57-1165-0388	538	1050.925	1276.35	33	33	35	27	-	1331.98	111.25	111.25	101.6	(2)	108	-	103	206	11	1 Right-hand helical gear $\alpha = 20^\circ$ ; $\beta = 6^\circ$	
62	1020	1268	90	3858	9E-1B30-1122-0455	212	1058	1185	17	M16	40	40	-	-	62	80	80	10	123	+0.9	77	154	13	2 Right-hand helical gear $\alpha = 14^\circ30'$ ; $\beta = 6^\circ$	
63	1057.15	1391.92	155.45	7887	9E-1B57-1223-0344	553	1120.775	1282.7	11/4 - 7 UNC	11/4 - 7 UNC	24	24	1060.45	1339.85	117.35	146.05	101.6	(2)	108	-	123	247	9; 15	3 Fixing holes on inner ring are divided on the circumference with spacing a' 360°/16	
64	1063.75	1366.5	130.05	6211	9E-1B45-1209-0468	400	1114.425	1257.3	1-8 UNC	1-8 UNC	35	30	1069.85	1314.45	104.65	114.3	76.2	(2)	106	-	77	154	8; 9	4 Gear Fellows Stub $\alpha = 20^\circ$	
65	1079.5	1450.34	114.3	6909	9E-1B50-1224-0370	495	1127.125	1320.8	27	27	35	28	1082.55	1365.25	101.6	114.3	101.6	(1.5)	84	-	120	240	11	5 Fixing holes on inner ring are divided on the circumference with spacing a' 360°/28	
66	1092.2	1377.7	101.6	5535	9E-1B40-1213-0433	335	1135.13	1290.07	23.8	23.8	36	36	-	1330.45	88.9	85.9	82.6	(2.5)	134	-	74	148	15	6 Centering diameter is on the opposite bearing face	
67	1095	1380	110	5535	9E-1B40-1212-0478	348	1135	1290	23	23	36	36	1100	1330	101	101	93	10	136	-	74	148	23	7 Fixing holes on inner ring are divided on the circumference with spacing a' 360°/24	
68	1680	2028	120	8461	9E-1B40-1830-0521	620	1745	1915	30	30	48	48	-	-	100	90	90	10	200	+0.4	72	144		8 Gear Involute Stub $\alpha = 20^\circ$	

- 9 Non-through tapped fixing holes on both rings
- 10 Gear Fellow Stub Tooth System Special-Full Fillet Radius  $\alpha = 20^\circ$
- 11 Fixing holes on inner ring are divided on the circumference with spacing a' 360°/36
- 12 Fixing holes on inner ring are recessed on  $\varnothing 50$  into the depth of 6.35
- 13 Non-through tapped fixing holes on outer ring
- 14 Fixing holes on both rings ring are recessed on  $\varnothing 30$  into the depth of 19.1
- 15 Gear Agma Stub  $\alpha = 20^\circ$
- 16 Fixing holes on inner ring are divided on the circumference with spacing a' 360°/30 (two places a' 180° are not occupied)
- 17 Fixing holes on inner ring are recessed on  $\varnothing 21$  into the depth of 11.5
- 18 Fixing holes on inner ring are divided on the circumference with spacing a' 360°/30
- 19 Fixing holes on inner ring are divided on the circumference with spacing a' 360°/40
- 20 Fixing holes on outer ring are recessed on  $\varnothing 41.3$  into the depth of 28.6
- 21 Gear Involute Stub-Full Fillet radius  $\alpha = 20^\circ$
- 22 Fixing holes on inner ring are divided on the circumference with spacing a' 360°/52
- 23 Fixing holes on both rings ring are recessed on  $\varnothing 34$  into the depth of 16

# FOUR-POINT CONTACT BALL SLEWING RINGS

-with internal gear [ I ]



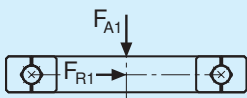
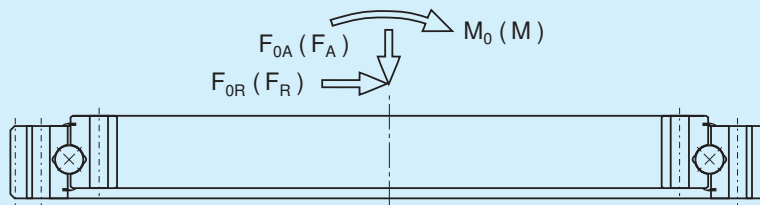
Number of the Loading Curve	Boundary Dimensions			Static Ax. Basic Load Rating $C_{0a}$	Designation	Weight G	Abutment Dimensions				Other Specifications										Permissible circumferencial force		Note No.	Notes
	d	D	T				$J_1$	$J_2$	$N_1$	$N_2$	$n_1$	$n_2$	$d_1$	$D_1$	H	B	$B_1$	m(DP)	z	x	$F_{TDov}$	$F_{TmaxDov}$		
	[mm]			[kN]		[kg]	[mm]				[mm]										[kN]			
69	256.95	418	50	708	9I-1B20-0342-0351	25	295	390	5/8-11 UNC	5/8-11 UNC	24	18	-	-	44	44	44	(5/7)	52	-	27	54	1	1 Gear Fellow Stub Tooth System $\alpha = 20^\circ$
70	323.8	520.5	54	1140	9I-1B25-0422-0283	46	365.1	479.4	5/8-11 UNC	5/8-11 UNC	20	20	-	-	52.3	52.3	52.3	(5/7)	65	-	29	58	1; 2	2 Non-through tapped fixing holes on both rings
71	380	545	55	988	9I-1B20-0465-0136	38	420	510	M12x1.25	13	16	16	400	-	45	45	40	4	96	-0.375	14	28	3	3 Non-through tapped fixing holes on inner ring
72	427.99	654.05	69.85	1533	9I-1B25-0560-0467	84	495.3	622.3	5/8-11 UNC	17.5	24	18	-	-	60.45	60.45	60.45	(4)	69	-	34	69	3; 4	4 Gear Involute Stub $\alpha = 20^\circ$
73	427.99	663.45	80.26	1995	9I-1B32-0560-0449	101.5	495.3	628.65	3/4-10 UNC	20.1	24	18	-	660.4	69.09	76.2	76.2	(4)	69	-	44	88	3; 4	5 Fixing holes on outer ring are divided on the circumference with spacing a' 360°/52
74	428	670	69.85	1533	9I-1B25-0559-0496	88.5	495.3	628.65	3/4-10 UNC	20.6	30	24	-	-	60.45	60.45	60.45	(4)	69	-	34	69	3; 4	6 Centering diameter $\varnothing$ 1011.2 is on both sides of the ring (on the front face into the depth of 1. on the opposite face into the depth 9.4)
75	546	716	69	1382	9I-1B20-0644-0135	55	605	690	M12	13.5	40	40	-	-	46	60	60	6	93	-	31	63	3	7 Gear Involute Stub-Full Fillet Radius $\alpha = 20^\circ$
76	560	825	90	3095	9I-1B36-0715-0317	137.5	645	785	M20	22	44	43	-	-	78	78	78	10	57	-0.5	90	180	5	8 Opposite face of the inner ring is fitted on $\varnothing$ 1010.92 into the depth 7.11
77	619.76	910.06	87.88	3515	9I-1B40-0780-0454	182	700	859.99	3/4-10 UNC	20.6	30	30	-	907.16	79	79	79	(3.5)	87	-	50	101	4	9 Gear Involute Modification Stub-Full Fillet Radius $\alpha = 20^\circ$
78	633	870	72	2572	9I-1B29-0761-0411	121	697	825	3/4-10 UNC	3/4-10 UNC	36	30	-	-	63	63	63	(4)	101	-	34	69	2; 4	10 Fixing holes on outer ring are divided on the circumference with spacing a' 360°/36
79	633	870	92	3011	9I-1B35-0761-0414	160	697	825	3/4-16 UNF	3/4-16 UNF	36	30	-	-	83	83	83	(4)	101	-	34	69	2; 4	
80	648.2	851	70	2123	9I-1B25-0763-0186	95	705	820	M16	M16	24	24	677	850	55	60	55	6	109	-0.5	38	76		
81	650.24	848.36	55.88	1588	9I-1B20-0741-0400	82	701.8	812.8	1/2-13 UNC	17.5	28	15	-	-	45.7	45.7	45.7	(4)	104	-	23	47	3; 4	
82	656	868	77	2009	9I-1B22-0782-0444	104	730	834	M16	18	24	24	694	-	55	68	64	8	82	-1	49	98		
83	670	857	88.9	2122	9I-1B25-0762-0391	120	727.075	822.325	3/4-10 UNC	3/4-10 UNC	24	20	696.97	-	73.15	86.1	51.05	(4)	107	-	28	56	2; 4	
84	736	950	70	2403	9I-1B25-0860-0157	98.5	805	920	M16	M16	30	30	775	-	55	60	55	8	94	-	46	92		
85	786.54	990.6	114.3	3267	9I-1B32-0897-0198	170	849.884	944.118	3/4-10 UNC	3/4-10 UNC	30	30	820.42	-	85.85	90.42	50.8	(3.5)	110	-	38	76	2; 4	
86	786.7	990.6	114.3	3545	9I-1B35-0895-0415	168	849.884	944.118	3/4-10 UNC	3/4-10 UNC	30	30	817.4	-	85.85	90.42	76.2	(3.5)	110	-	47	95	2; 4	
87	944	1159	79	3021	9I-1B25-1065-0134	161	1015	1124	M16	17.5	36	36	-	-	54	70	70	8	118	-1	64	129	3	
88	945.4	1200	100	3781	9I-1B29-1103-0323	240	1040	1165	M20x1.5	21.5	36	36	-	-	80	82	82	12	80	-	95	190	3	
89	961	1177	90	3702	9I-1B30-1070-0372	181	1040	1134	5/8-11 UNC	17.8	36	36	1011.2	1174	77	80.5	70.1	(2.5)	94	-	75	150	3; 6	
90	957.07	1168.4	100.08	3970	9I-1B32-1087-0421	190	1039.88	1134.11	3/4-10 UNC	3.4-10 UNC	36	36	1005.84	1165.35	83.06	83.06	55.12	(2.5)	96	-	58	117	2; 7; 8	
91	957.07	1168.4	119.38	4977	9I-1B40-1086-0450	205	1039.88	1134.11	3/4-10 UNC	3/4-10 UNC	36	36	1005.84	1165.35	93.98	95.25	55.12	(2.5)	96	-	58	117	2; 7	
92	1007.87	1298.45	90.42	4277	9I-1B32-1167-0504	282	1092.2	1247.775	1-8 UNC	27	20	22	1057.15	-	79.25	68.33	65.79	(2.5)	100	-	69	139	3; 9	
93	1048.51	1320.8	128.52	6037	9I-1B45-1187-0352	349	1130.18	1279.52	7/8-9 UNC	23.8	40	36	1091.44	-	50.8	119.13	101.6	(2.5)	104	-	107	214	3; 9	
94	1060.7	1339.85	121.41	5534	9I-1B40-1204-0197	361	1149.35	1295.4	1-8 UNC	27	30	30	1104.9	1336.55	98.55	104.9	76.2	(2.5)	106	-	67	134	3; 4	
95	1071	1305	98	4408	9I-1B32-1200-0392	245	1156	1265	M16	21	48	48	1120	-	82	90	88	10	106	-1.5495	102	204	3	
96	1083.6	1310	110	4172	9I-1B29-1213-0324	243	1170	1275	M20x1.5	21.5	36	36	-	-	80	94	94	14	79	-	127	254	3	
97	1140	1404	112	3667	9I-1B25-1296-0180	303	1232	1360	M20	22	48	48	-	-	70	103	103	10	115	-0.5	119	238		
98	1162	1460	120	5905	9I-1B38-1340-0325	402	1270	1420	M24x2	25	36	35	1227	-	95	105	98	14	85	-	131	263	3; 10	
99	1610	2000	150	12609	9I-1B60-1830-0267	885	1720	1940	30	30	54	54	1665	-	125	125	100	12	135	-0.5	139	278		

# SELECTION OF SLEWING RING TYPE AND SIZE

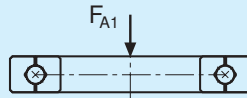
Selection of a suitable slewing ring for common applications can be carried out from the point of view of the static load rating by means of the diagrams (curves) for the limiting static load of the raceways and fixing bolts (pages 32 - 62 of this publication) based on the calculated equivalent axial and moment static load.

Slewing rings allow accommodation of combined loads, i.e. both axial and radial forces and tilting moments including eccentric loads. Typical examples of loading are shown in the following table.

## Loading - Typical Examples



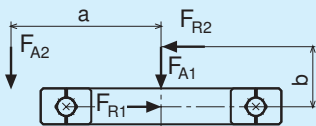
$$\begin{aligned} F_A &= F_{A1} \\ F_R &= F_{R1} \\ M &= 0 \end{aligned}$$



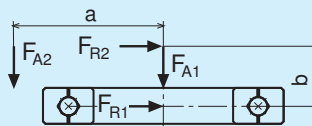
$$\begin{aligned} F_A &= F_{A1} \\ F_R &= 0 \\ M &= 0 \end{aligned}$$



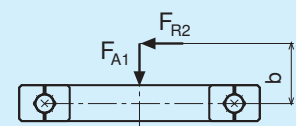
$$\begin{aligned} F_A &= 0 \\ F_R &= F_{R1} \\ M &= 0 \end{aligned}$$



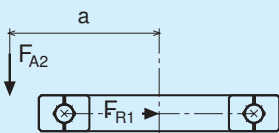
$$\begin{aligned} F_A &= F_{A1} + F_{A2} \\ F_R &= |F_{R2} - F_{R1}| \\ M &= F_{A2} \cdot a + F_{R2} \cdot b \end{aligned}$$



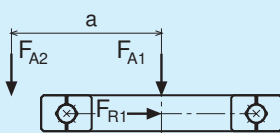
$$\begin{aligned} F_A &= F_{A1} + F_{A2} \\ F_R &= F_{R1} + F_{R2} \\ M &= |F_{A2} \cdot a - F_{R2} \cdot b| \end{aligned}$$



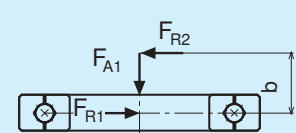
$$\begin{aligned} F_A &= F_{A1} \\ F_R &= F_{R2} \\ M &= F_{R2} \cdot b \end{aligned}$$



$$\begin{aligned} F_A &= F_{A2} \\ F_R &= F_{R1} \\ M &= F_{A2} \cdot a \end{aligned}$$



$$\begin{aligned} F_A &= F_{A1} + F_{A2} \\ F_R &= F_{R1} \\ M &= F_{A2} \cdot a \end{aligned}$$



$$\begin{aligned} F_A &= F_{A1} \\ F_R &= |F_{R2} - F_{R1}| \\ M &= F_{R2} \cdot b \end{aligned}$$

### Calculation of Equivalent Axial and Moment Static Load

Slewing Rings	Formula	Valid if
Four-Point Contact Ball Slewing Rings	$F'_{OA} = (F_{OA} + 5.05 \cdot F_{OR}) \cdot s_O$ $M'_{OK} = M_{OK} \cdot s_O$	$0.1 < \frac{F_{OR}}{F_{OA}} < 8$ $e > 2$
	$F'_{OA} = (1.23 \cdot F_{OA} + 2.68 \cdot F_{OR}) \cdot s_O$ $M'_{OK} = 1.23 \cdot M_{OK} \cdot s_O$	$0.1 < \frac{F_{OR}}{F_{OA}} < 8$ $e \leq 2$
Crossed Roller Slewing Rings	$F'_{OA} = (F_{OA} + 2.05 \cdot F_{OR}) \cdot s_O$ $M'_{OK} = M_{OK} \cdot s_O$	$0.1 < \frac{F_{OR}}{F_{OA}} < 8$

Where:  $F_{OA}$  -  $\Sigma$  of axial static forces for slewing ring [kN]  
 $F_{OR}$  -  $\Sigma$  of radial static forces for slewing ring [kN]  
 $M_{OK}$  -  $\Sigma$  of tilting moments for slewing ring (static) [kNm]  
 $s_O$  - coefficient of static safety (values - see Table 3) [-]  
 $e = \frac{2000 \cdot M_{OK}}{F_{OA} \cdot D_S}$  - parameter of the load eccentricity [-]  
 $D_S$  - slewing ring mean diameter [mm]

Note: - if:  $\frac{F_{OR}}{F_{OA}} < 0.1$  - when calculating the equivalent load, radial force need not be taken into account.

The calculated values of the axial and moment static load define the coordinates of the working point in the diagram for the limiting static load of the slewing ring. The working point must lie under the curve for the bolt static load. Example - see chapter DIAGRAMS FOR LIMITING STATIC LOAD, page 31.

Suitability for a given application from the point of view of gear dimensioning can be evaluated by comparison of the real nominal and maximal circumferential forces with allowed circumferential forces for the gear. Allowed nominal and maximal circumferential forces - Slewing Ring Tables.

Calculation of the nominal and maximal circumferential force:

$$F_{Tmen} = \frac{2000 \cdot M_{Tmen}}{m \cdot (z + 2x)}$$

$$F_{Tmax} = \frac{2000 \cdot M_{Tmax}}{m \cdot (z + 2x)}$$

Where:

$F_{Tmen}$  - nominal circumferential force [kN]  
 $F_{Tmax}$  - maximal circumferential force [kN]  
 $M_{Tmen}$  - nominal rotating moment [kNm]  
 $M_{Tmax}$  - maximal rotating moment [kNm]  
 $m$  - gear module [mm]  
 $z$  - number of teeth [-]  
 $x$  - unit displacement of the basic profile (unit correction) [-]

The main criteria for evaluating of the gear suitability is the fatigue resistance of bending and max. static load transmission. Following conditions must be fulfilled:

$F_{Tmen} \leq F_{TDov}$  - for fatigue resistance of bending (values - see Slewing Ring Tables)  
 $F_{Tmax} \leq F_{TmaxDov}$  - for max. static load transmission (values - see Slewing Ring Tables)



Figure 1

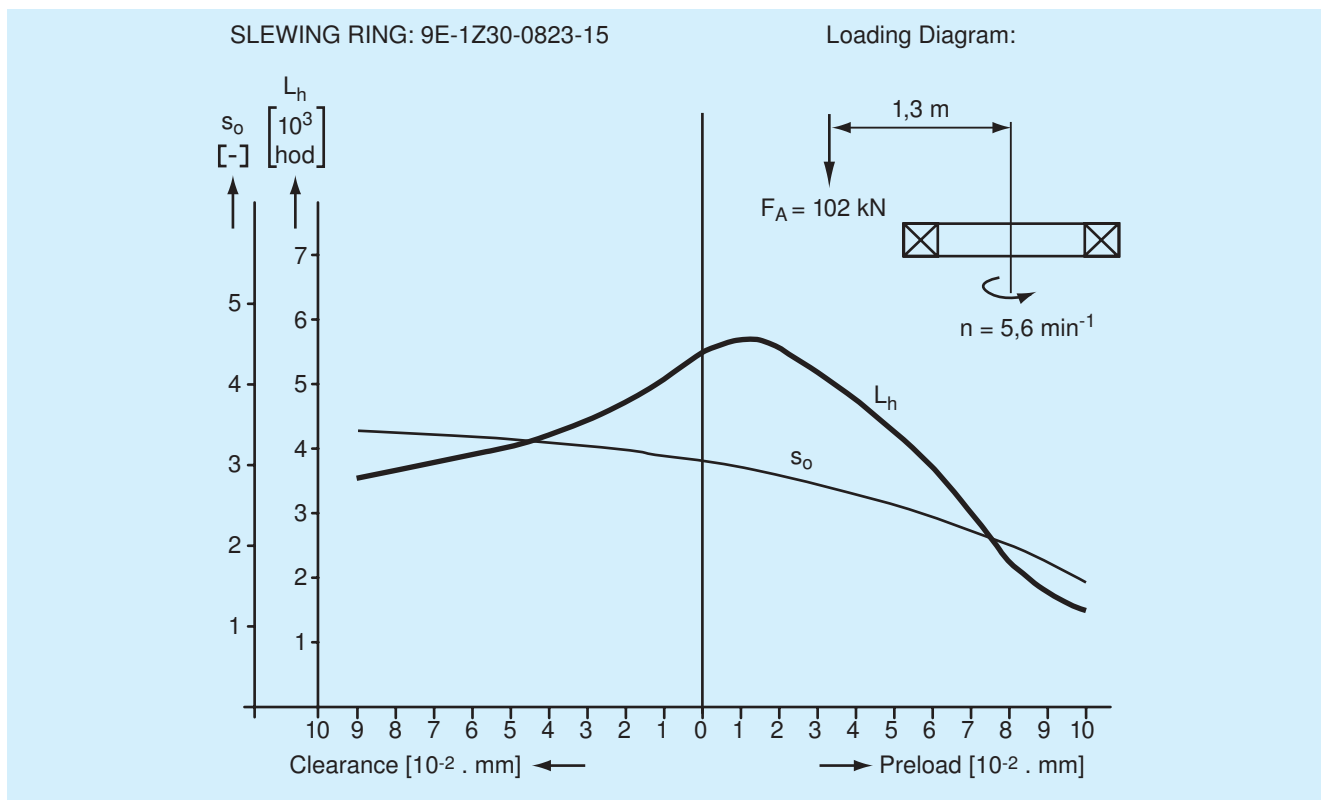
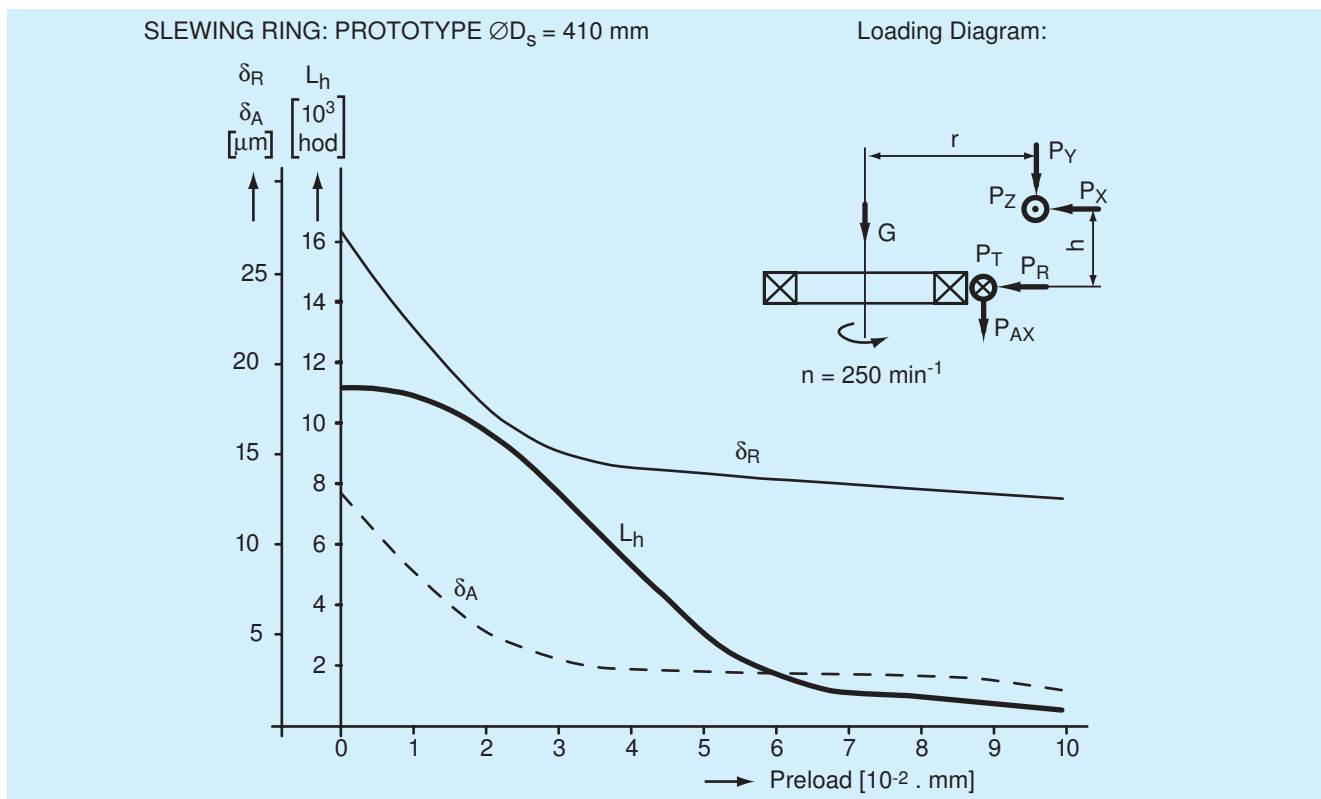
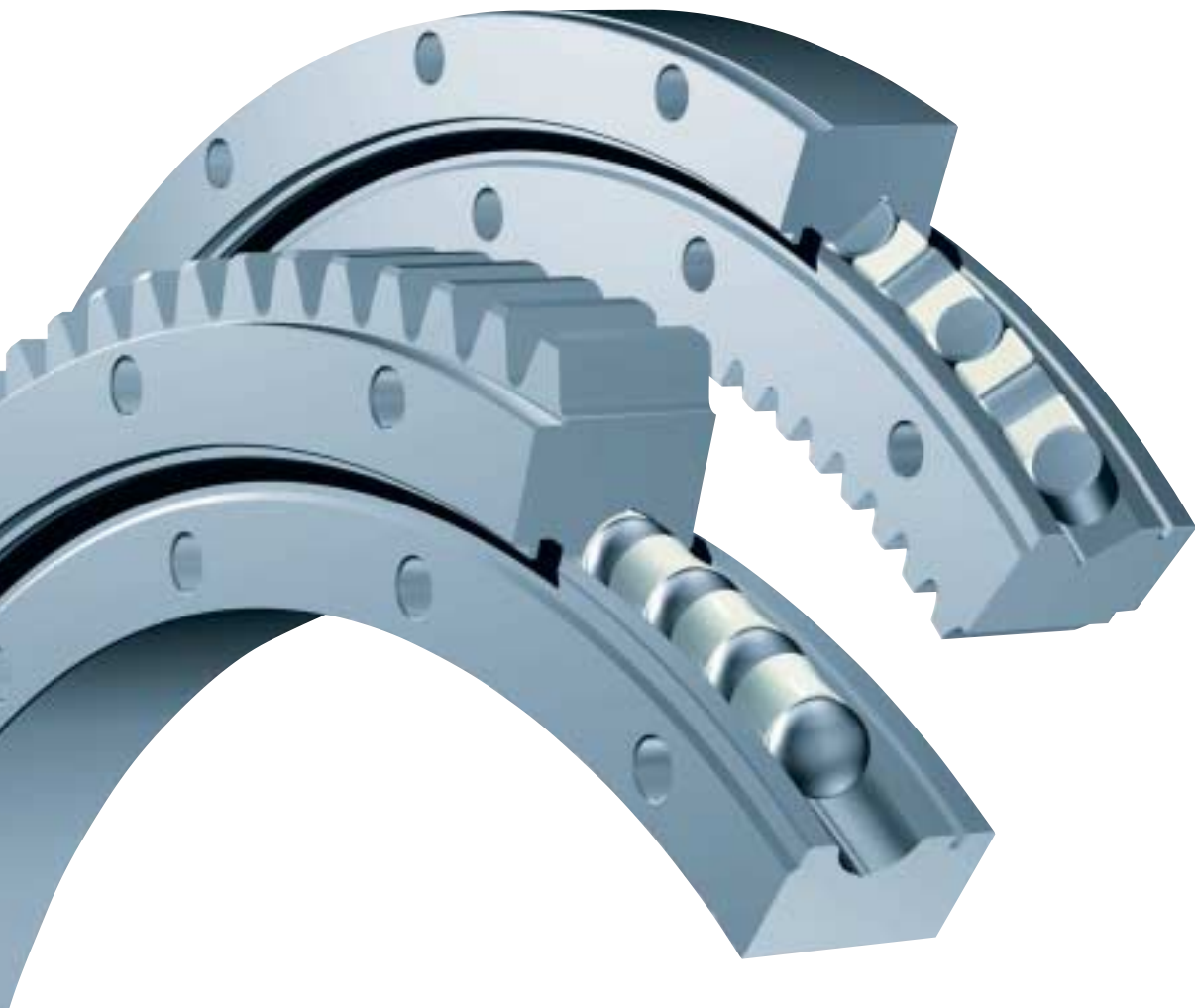


Figure 2





## SLEWING RING CHARACTERISTICS, APPLICATIONS

Slewing rings are large-sized bearings which are able to accommodate combined load, i.e. axial, radial loads and tilting moment. They are usually provided with holes for fixing bolts, internal or external gear, lubrication holes and seals, which allow a compact and economical arrangement. They often enable elimination of many components necessary in the classical bearing arrangement.

PSL slewing rings have proven ability in the following applications

- construction, mobile and pillar cranes,
- shovel, digging-wheel excavators,
- revolving grabs and winches,
- graders,
- logging industry machines,
- loaders, vehicles for waste removal, hydraulic grippers,
- axles and undercarriages,
- assembly and access platforms,
- robots, manipulators and positioners,
- machine tools,
- special equipment (rescue vehicles, aeriels, feller bunchers and tunnel machines, drilling equipment, wind-power plants, cleaning and bottle filling machines).

Compactness, accuracy and smooth operation with relatively high rigidity, together with simple mounting and reliability in operation are qualities that allow the use of these bearings in all industrial branches.

